

Effect of Nano-ZrO₂ Reinforcement on the Physical, Thermal, and Electrical Properties of Aluminum 7075 Alloy

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Abstract:

The research deals with improving the thermal, electrical, and physical properties of 7075 aluminum alloy using nano zirconium oxide (ZrO₂) as reinforcement. The composite materials were prepared using the powder metallurgy technique to achieve a homogeneous distribution of the reinforcement particles. The effect of different percentages of ZrO₂ (0.5%, 1%, 1.5%, and 2%) on the alloy was studied. The study included physical tests (density, porosity), structural analyses (XRD, SEM), as well heat conversion and electrical properties. The results XRD showed the peaks in the Al7075/ZrO₂ composite are shifted to a lower 2θ. it proved the SEM, that the ZrO₂ reinforcement particles were evenly distributed. The apparent density increased from 4.7 to 5.4 g/cm³, while the bulk density increased from 2.8 to 3.8g/cm³, the apparent porosity decreased from 39 to 16%, while the true porosity decreased from 33 to 14 %. The thermal conductivity decreased from 130 w/m. k to 109 w/m. k, and the electrical conductivity decreased from 25x10⁶ s/m to 20x10⁶ s/m. with increasing ZrO₂ content.

Keywords: Al7075 alloy, Nano ZrO₂, Powder metallurgy, Thermal properties, Electrical conductivity, Porosity, density.

تأثير التدعيم باستخدام أكسيد الزركونيوم النانوي على الخواص الفيزيائية والحرارية والكهربائية لسبائك الألومنيوم 7075

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مستخلص:

يتناول البحث تحسين الخصائص الحرارية والكهربائية والفيزيائية لسبائك الألومنيوم 7075 باستخدام أكسيد الزركونيوم النانوي (ZrO₂) كتدعيم. تم تحضير المواد المركبة باستخدام تقنية مسحوق المعادن لتحقيق توزيع متجانس لجزيئات التدعيم. تمت دراسة تأثير النسب المئوية المختلفة من ZrO₂ (0.5٪، 1٪، 1.5٪، و 2٪) على السبيكة. تضمنت الدراسة الاختبارات الفيزيائية (الكثافة، المسامية)، والتحليلات البنيوية (XRD، SEM)، وكذلك التحويل الحراري والخصائص الكهربائية. أظهرت نتائج XRD أن القمم في المركب Al7075 / ZrO₂ قد تحولت إلى 2θ أقل. أثبت فحص المجهر الإلكتروني الماسح، أن جزيئات التدعيم ZrO₂ موزعة بالتساوي. زادت الكثافة الظاهرية من 4.7 إلى 5.4 g/cm³، بينما زادت الكثافة الظاهرية من 2.8 إلى 3.8 g/cm³، انخفضت المسامية الظاهرية من 39 إلى 16٪، بينما انخفضت المسامية الحقيقية من 33 إلى 14٪. وانخفضت الموصلية الحرارية من 130 إلى 109 w/m.k، وانخفضت الموصلية الكهربائية من 25*10⁶ إلى 20*10⁶ s/m مع زيادة محتوى أكسيد الزركونيوم.

الكلمات المفتاحية: سبائك 7075، أكسيد الزركونيوم النانوي، ميتالورجيا المساحيق، الخواص الحرارية، التوصيل الكهربائي، المسامية، الكثافة.

1. Introduction

Aluminum 7075 is a widely used aerospace-grade alloy, celebrated for its high strength-to-weight ratio, excellent fatigue resistance, and machinability. Despite its superior mechanical properties, certain applications demand further enhancements in thermal stability, electrical conductivity, and physical characteristics. This has driven the exploration of advanced composite materials reinforced with nanoscale ceramics, such as nano-zirconium oxide (ZrO₂) [1].

Nano-ZrO₂ is renowned for its remarkable thermal stability, corrosion resistance, and mechanical robustness. When integrated into metal matrices like Aluminum 7075, it can significantly enhance the material's performance, addressing limitations in extreme operating environments. For instance, the thermal properties of ZrO₂ contribute to improved heat dissipation, while its structural reinforcement enhances wear resistance and overall mechanical stability. Additionally, the electrical properties of the composite can be fine-tuned, potentially broadening its application in advanced electronic and

aerospace systems [2].

Research in this area highlights the synergistic effects of nano-ZrO₂ inclusions on aluminum alloys, revealing promising improvements in hardness, tensile strength, and thermal conductivity. Such advancements underscore the potential of nano-ZrO₂-reinforced composites in critical sectors, including aerospace, automotive, and energy industries. This study aims to explore these enhancements in detail, contributing to the growing body of knowledge on nanocomposite materials [3].

Powder metallurgy (PM) has emerged as a leading manufacturing technique for these composites due to its ability to produce uniform dispersions of reinforcement particles. This process involves mixing aluminum powder with nano-ZrO₂ particles, followed by compaction and sintering under controlled conditions. Powder metallurgy allows precise control over particle distribution and density, which are critical for achieving optimal material properties. Additionally, it minimizes material wastage and allows for the production of complex shapes with tailored properties. Studies have demonstrated that composites

produced via PM exhibit superior mechanical and thermal characteristics compared to those manufactured using conventional methods. This makes PM an attractive choice for the industrial-scale production of nano-ZrO₂-reinforced Aluminum 7075 composites [4, 5, 6].

This study is to investigate the effects of nano-ZrO₂ reinforcement on the thermal, electrical, and physical properties of Aluminum 7075 composites. This research seeks to establish a comprehensive understanding of the material behavior, thereby offering insights into the optimization of manufacturing processes. Ultimately, this work aspires to contribute to the de-

velopment of high-performance composites for applications in aerospace, automotive, and other high-demand sectors.

2. Experimental study

Raw Materials (Powders) Used:

The powders were utilized in the preparation of the composite material, with aluminum alloy (AL7075) serving as the matrix material. Table (1) presents the specifications of the powders used, including their purity, particle size, origin, density, and proportions. The reinforcement material is the nano-oxide: zirconia (ZrO₂), Table (2) provides the specifications of the nano-oxide powder as well.

**Table (1): Specifications of Powders
for Aluminum Alloy (Al7075) Prepared Using Powder Metallurgy**

Powder Type	Purity (%)	Particle Size (nm)	Origin	Density (g/cm ³)	Proportion (%)
Aluminum (Al)	99.5	≥63	Indian	2.81	90
Zinc (Zn)	99.5	≥63	Indian	7.14	5.67
Magnesium (Mg)	99.5	≥63	Indian	1.74	2.5
Copper (Cu)	99.5	≥63	Indian	8.96	1.6
Chromium (Cr)	99.5	≥63	Indian	7.19	0.23

Table (2): Specifications of Nano-Oxide Powders of American Origin

Powder Type	Purity (%)	Particle Size (nm)	Origin	Density (g/cm ³)
Nano Zirconium Oxide (ZrO ₂)	100	≥50	American	5.89

Powers Mixing

The powders were mixed thoroughly in a steel container and steel balls with a diameter of (10 mm) were placed and formed with a homemade electric mixer. The powders were mixed in the proportions given in Table (1) to prepare

the aluminum alloy (AL7075). The reinforcement powders were also mixed and blended by adding different weight proportions of nano oxides with the base material (AL7075) as in Table (3) and were mixed well to obtain a homogeneous mixture.

Table (3): The weight percentages for each composite

		Al7075	A1	A2	A3	A4
Composite	Al 7075	100	99.5	99	98.5	98
	ZrO ₂	0	0.5	1	1.5	2

Powder Pressing

After weighing the materials and mixing them accurately to obtain a homogeneous powder, the samples were pressed and formed using the Unix-axil pressing method using a steel mold made of steel with a diameter of (10mm). After that, the well-mixed powder was placed inside the mold and

the mold was placed inside the German-made hydraulic press of the type (DK 7510 BARRIT DENMARK) with a pressing capacity of (40Ton) and a load of (8Ton) was applied for (30 Sec), to ensure that elastic return does not occur, and to obtain cylindrical samples with a diameter of (10mm).



Figure 1: The samples obtained after pressing the powders

Sintering

The thermal sintering process was carried out using a German-made (QUAYLE DENTAL) electric furnace that reaches a temperature of (900°C). A (65cm) long tube made of heat-resistant stainless steel was used, open at one end and closed at the other end with a plug of thermal clay. It was connected to an electric discharge device (Rotary Pump) that was used to obtain a high discharge to prevent oxidation of the samples during the thermal sintering process. The furnace temperature was raised to (500°C), which is the sintering temperature, while the samples were kept inside the furnace for an hour and a half, then the furnace was turned off, and the samples were kept inside the furnace until the next day until the samples cooled slowly inside the furnace to room temperature.

3. Examinations and Testing

Structural characterization

After sintering, the samples were smoothed and polished using polishing papers with grit sizes ranging from 2000 to 4000 to achieve a fine surface finish. The microstructural characterization of the samples was performed by

performing XRD and FESEM analyses. Characterization. The XRD analysis of the samples was performed using X-ray diffraction testing was conducted using a device of type (x'Peart Highscore Plus) of Dutch origin. with a scan rate of 4°/min and a step size of 0.02° with CuK α radiation ($\lambda = 1.5405 \text{ \AA}$). The morphology of the samples was analyzed by FESEM Type (TESCAN), Model (MIRA3), and French origin.

Physical Tests

Physical assessments were performed, encompassing apparent and volumetric density, apparent and real porosity, in addition to water absorption. The tests were performed utilizing the Archimedes principle approach in accordance with the international standard (ASTM C373-88) [7]. An accurate German-made electric balance with a precision of (0.0001g) was employed, following these steps: -

1- The samples were subjected to drying for one hour in an electric oven at a temperature of 100°C, remaining in the oven until they cooled. Upon extraction from the oven, the samples were weighed to determine the dry weight (Wd).

2- The samples were submerged for

24 hours in a vessel containing distilled water at ambient temperature. The samples were subsequently extracted from the water, and only the water droplets adhering to the surface of the samples were eliminated. The samples were subsequently weighed to determine the saturated weight (W_s).

3- The materials were weighed in distilled water using a precise suspension balance to determine the suspended weight (W_i).

In order to determine water absorption, apparent porosity, bulk density, saturated weight, and dry weight, one must first know the three weights. The following relationships are used to calculate them:

$$T.D = \sum_{i=1}^n (\rho_i \cdot X_i) \dots\dots\dots (1)$$

Where: T.D: theoretical density, ρ_i : theoretical density of the elements composing the single body (g/cm³), X_i : percentage of each element in the body.

$$\rho_a = \left(\frac{W_d}{W_d - W_i} \right) * \rho_w \dots\dots\dots (2)$$

Where: ρ_a : Apparent Density (g/cm³), ρ_w : Density of water (g/cm³), W_d = dry weight of the body (g), W_i = weight of the body suspended in water (g).

$$\rho_b = (W_D / (W_s - W_i)) * \rho_w \dots\dots\dots 3$$

Where: ρ_b : bulk density (g/cm³), W_s : weight of the body saturated with water (g).

$$A.P. = \frac{W_s - W_d}{W_s - W_i} * 100\% \dots\dots\dots 4$$

Where: A.P: Apparent Porosity

$$T.P. = \frac{T.D. - B.D.}{T.D.} * 100\% \dots\dots\dots (5)$$

Where: T.P.: Total porosity ratio of the sintered body, T.D.: theoretical density of the sintered body (g/cm³).

$$W.A = W_s - \frac{W_d}{W_d} * 100\% \dots\dots\dots (6)$$

Where: W.A: Water Absorption Capacity.

Electrical Conductivity Test

The electrical conductivity test was performed using an American-made LCR-Meter, type (Precision Impedance, Analyzer Agilent 4294A, USA). The electrical conductivity was calculated from the following relationship, and the electrical resistance was calculated from the reciprocal of the electrical conductivity.

$$\sigma_{A.C} = 2\pi f \epsilon_0 \epsilon'' \dots\dots\dots (7)$$

Where: ϵ_0 is the permittivity of vacuum and its value is 8.854×10^{-12} F/m, f Frequency in HZ for each sample

$$\rho_{a.c} = \frac{1}{\sigma_{a.c}} \quad \text{..... (8)}$$

Thermal Conductivity Test

The thermal conductivity test was conducted using a Heat conversion unit manufactured by P.A. Hilton Ltd England. The thermal conductivity coefficient (K) is calculated from the Fourier Law equation:

$$-k = \frac{Q}{A \times \frac{\Delta T}{\Delta X}} \quad \text{..... (9)}$$

Where: k: Thermal conductivity coefficient (w/m.k), Q: The amount of heat passing through per unit time (w), A: Cross-sectional area of heat flow (m²), $\Delta T/\Delta X$: Thermal gradient with respect to distance (k/m).

4. Results and discussion

Microstructural analysis

X-Ray diffraction of Al7075/ZrO₂ composites

Reinforced Al7075 with ZrO₂ particles at varying percentages (0.5, 1, 1.5, and 2%), the XRD pattern of the resulting Al7075/ZrO₂ composite is displayed in Figure 3. Zirconia and aluminum peaks can be seen in the XRD pattern. which peaks grows as the weight fraction of ZrO₂ particles in-

creases. In contrast to the Al7075 material, the Al7075 peaks in the Al7075/ZrO₂ composite are somewhat shifted to a lower 2 θ . The stability of the Al7075/ZrO₂ composite is demonstrated by the XRD pattern. Adding ZrO₂ particles to Al7075 material does not result in the production of intermetallic compounds. The XRD pattern further proves that the ZrO₂ and Al7075 matrix materials are pure. As well as this aligns with [8].

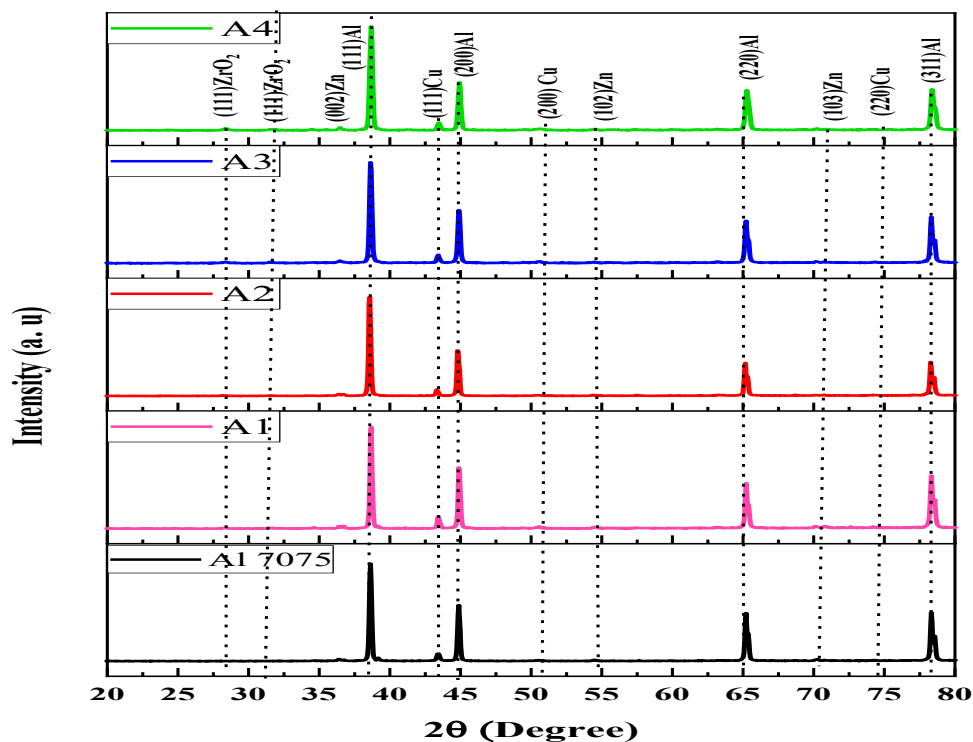


Figure 2: X-ray diffraction of Al7075 alloys the reinforcement with different proportions of ZrO₂.

SEM and EDX analysis

Composites with ZrO₂ (0.5, 1, 1.5, and 2 wt.%) reinforced particles and pure Al7075 are shown in SEM micrographs in Figure 3(a) and (b). It seems that the ZrO₂ particles in the Al7075 material have a spherical shape, as seen in the figure. Adding ZrO₂ particles to the composite causes the reinforcement particles to disperse evenly along the grain boundaries, as shown in the SEM micrographs. Additionally, it proved that the ZrO₂ reinforcement par-

ticles were evenly distributed, which decreased the likelihood of particle aggregation. The synthesis of composites, which involves powder milling, is responsible for this achievement [9]. Porosity in the Al7075/ZrO₂ composite is decreased due to the reduction of agglomeration and segregation, which is achieved by improving the uniform distribution of ZrO₂ reinforcement particles. As a result, the composites' mechanical behavior is enhanced [10]. In Figure 3(b), we can observe the composite Al7075/ZrO₂ energy-dispersive

spectra. The presence of aluminum, Zr, and O is demonstrated by the peaks, according to the EDS studies. As a result, we know that the composite con-

tains ZrO_2 particles. The composition of the Al7075/ ZrO_2 composite sample can be better understood with the use of this study.

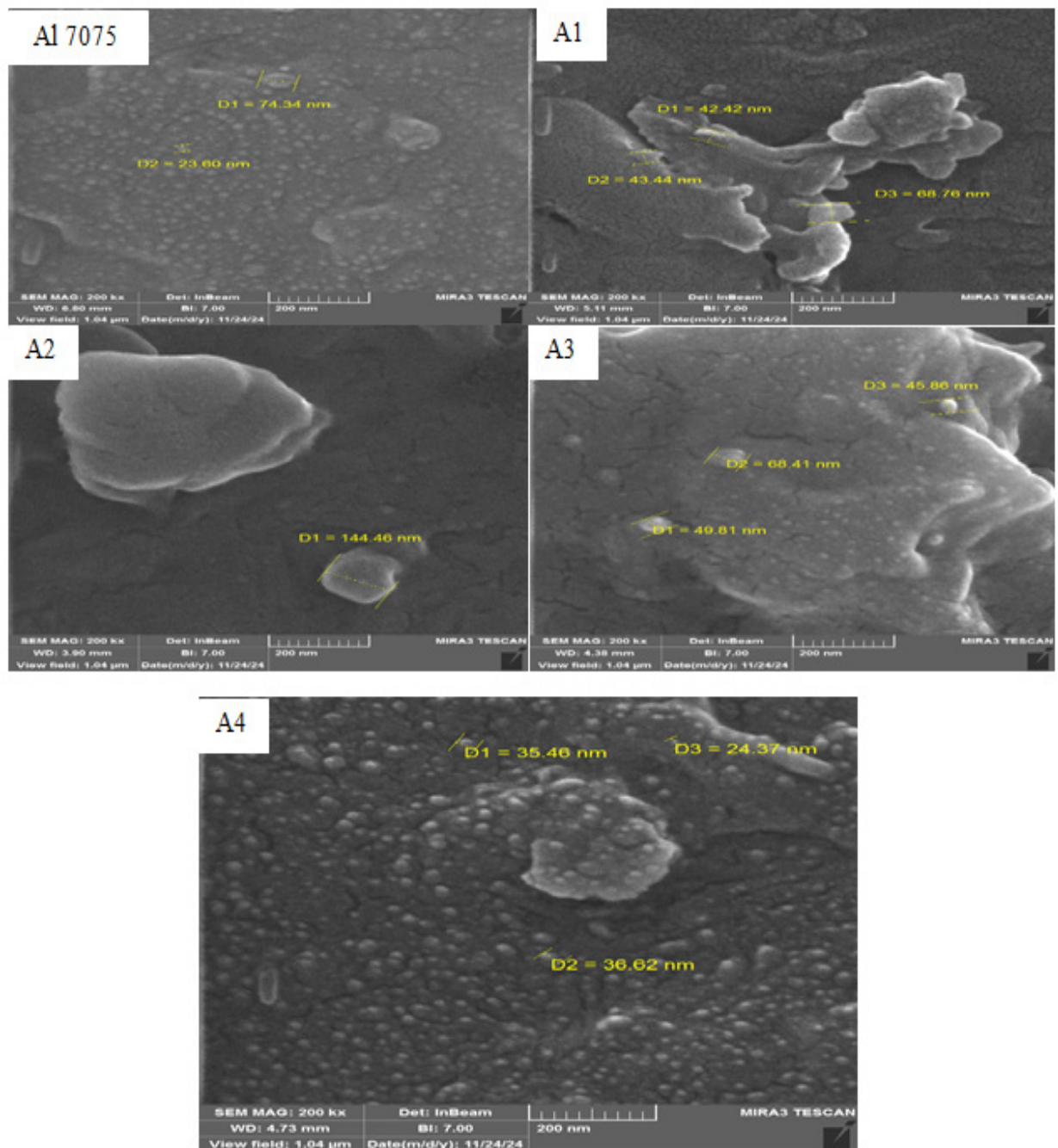


Figure 3 (a): show effect ZrO_2 content on SEM analysis of Al7075 alloys.

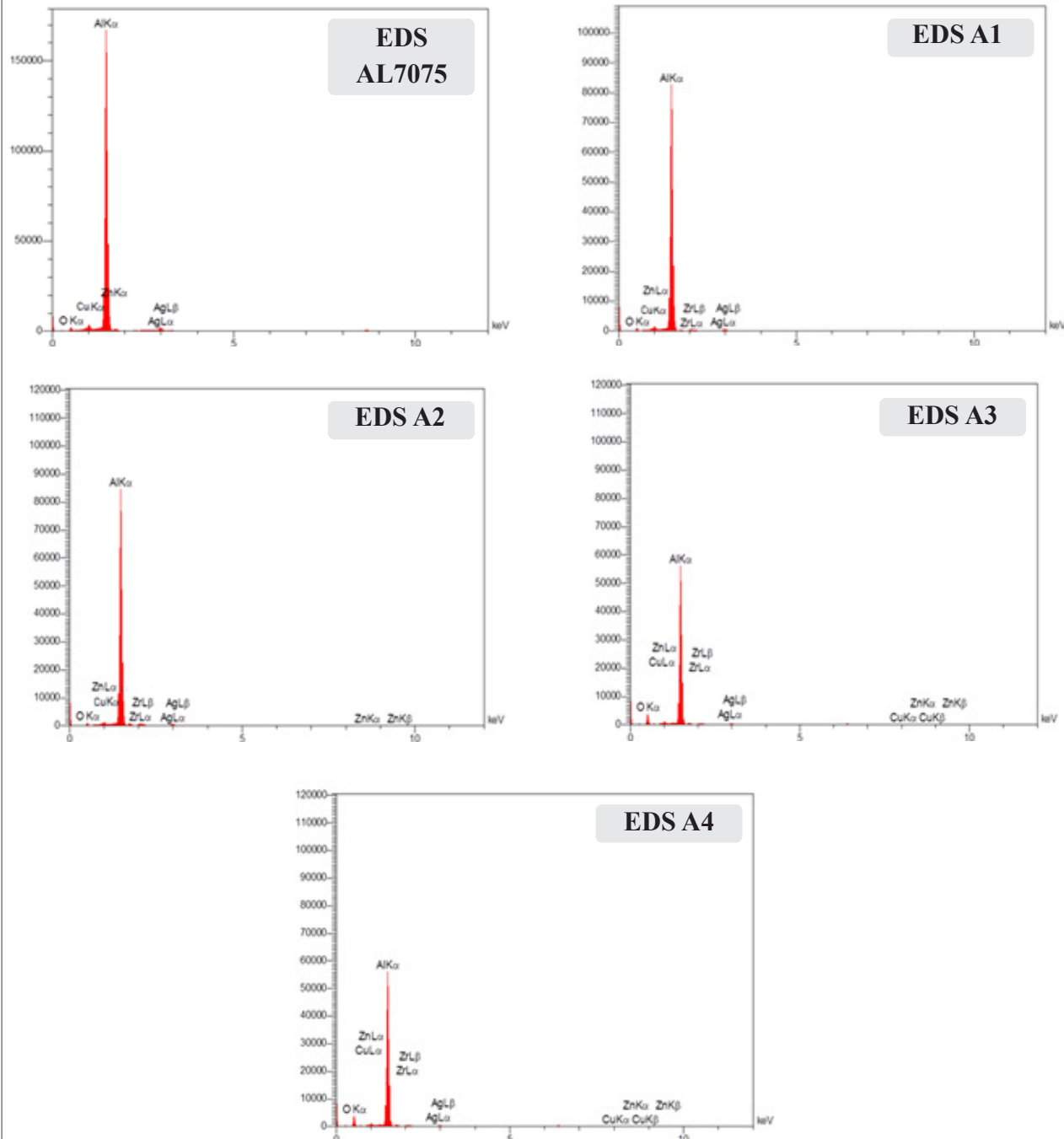


Figure 3 (b): show effect ZrO₂ content on EDS analysis of Al7075 alloys.

Physical properties:

Figure (4), shows the effect of adding zirconium dioxide (ZrO₂) on the

apparent density and bulk density of Al7075 aluminum alloy. The figure shows that increasing the ZrO₂ content leads to an increase in density. When

ZrO₂ is added in small amounts, it acts as a binding agent that improves the cohesion between the grains, which leads to a reduction in voids. At addition ratios (0.5%-1.5%), there a limited effect because the material has reached a metastable state where the structural effects begin to saturate. At higher ratios (1.5%-2%), the ZrO₂ particles are more uniformly distributed and the microstructure of the alloy is rearranged, improving the structural cohesion and hardness due to the enhanced inter-

penetration between the grains, which leads to a significant increase in density. The addition of ZrO₂ improves the order of the crystal lattice and reduces crystal defects (such as voids between particles) as a stabilizing agent, which leads to reduced porosity and increased density. In addition, ZrO₂ has a higher density than aluminum (ZrO₂ $\approx$ 5.68 g/cm³ compared to Al $\approx$ 2.7 g/cm³), and thus its incorporation leads to an increase in the density of the alloy, and this agrees with [11, 12].

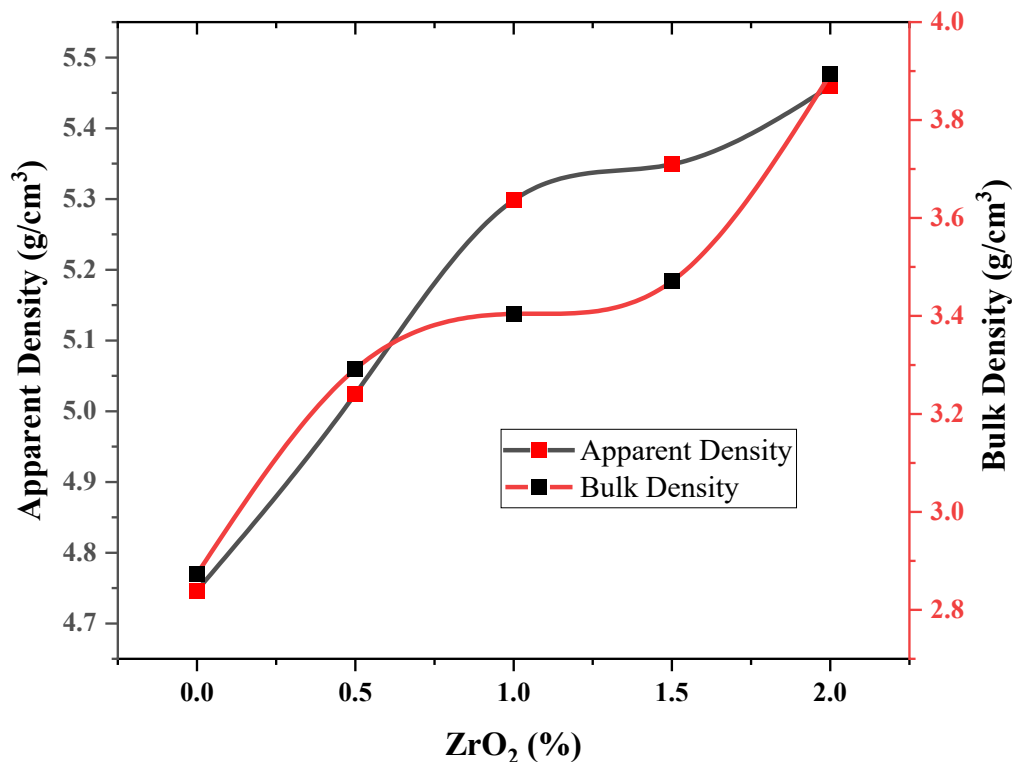


Figure 4: shows the effect of ZrO₂ content on Apparent and Bulk density for Al7075 Alloy.

Apparent and True Porosity

Figure (5) shows the effect of adding zirconia (ZrO₂) on both the apparent porosity and true porosity of Al7075 aluminum alloy. It is shown that the apparent porosity decreases with increasing zirconia content. At zirconia content (0%), the apparent porosity is about 40%. With increasing zirconia content to 2%, the apparent porosity decreases to about 15%. This is attributed to the

fact that adding zirconia improves the alloy structure by reducing the apparent porosity. The figure shows a similar decrease in true porosity with increasing zirconia content. The true porosity starts at about 35% at zirconia content (0%) and reaches about 10% at zirconia content (2%). This shows that the effect of zirconia extends to improving the material density and particle distribution within the alloy. And this agrees with [13, 14].

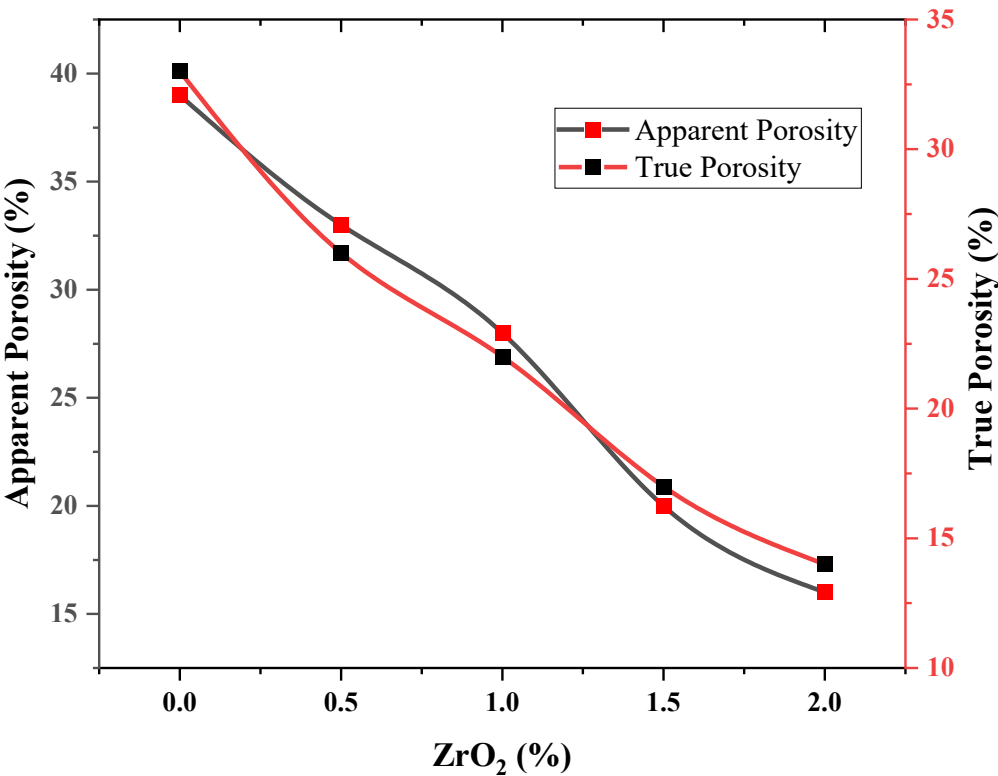


Figure 5: show the effect of ZrO₂ content on Apparent and True porosity for Al7075 Alloy.

Electrical and thermal properties

Figure (6a, b) shows the relationship between the percentage of adding (ZrO_2) to the Al7075 alloy and the thermal, and electrical conductivity of the alloy.

Figure (6, a) shows the decrease in the thermal conductivity of the alloy with the increase in the percentage of zirconium oxide. The conductivity decreased from (130 w/m.k) for the pure alloy to (109.2 w/m.k) at (2%) zirconium oxide. This decrease is attributed to the fact that zirconium oxide contributes to changing the microstructure of the alloy as zirconium oxide is distributed in the form of particles in the alloy, which hinders the movement

of electrons and phonons. With the increase in the zirconium oxide content, the thermally insulating regions in the material increase, which reduces the overall thermal conductivity of the alloy which agrees with [11].

Figure (6, b) shows the decrease in electrical conductivity with increasing zirconium oxide content in the aluminum alloy from (250×10^5 s/m) for the pure alloy to (20×10^5 s/m) at a content of (2%) zirconia oxide. This decrease is attributed to the fact that zirconium oxide particles act as impurities or dispersants within the crystal structure. They hinder the movement of free electrons. The electronic dispersion increases at the crystal boundaries. This agrees with [15].

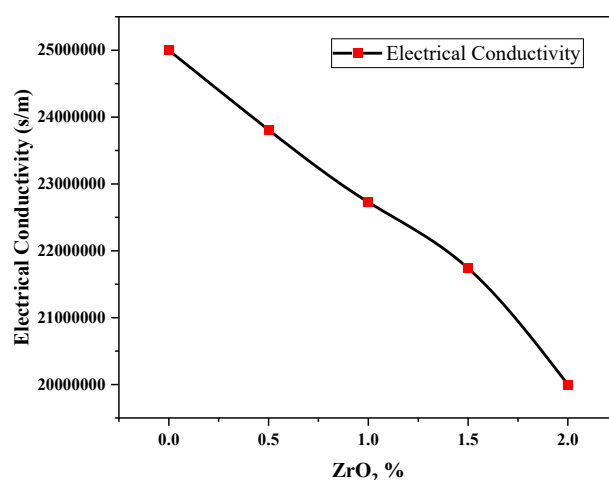
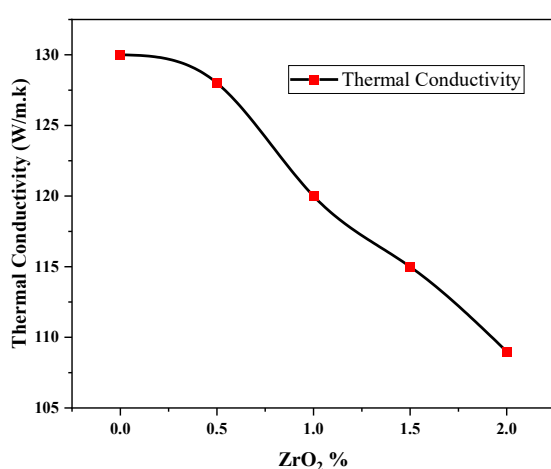


Figure 6(a, b): shows the effect of ZrO_2 content on Thermal, Electrical conductivity for Al7075 Alloy.

Conclusions:

XRD and SEM analyses revealed a uniform distribution of ZrO₂ particles within the alloy, leading to an enhanced crystal structure and reduced defects. The addition of ZrO₂ increased density and reduced both apparent and true porosity due to improved inter-grain bonding and minimized voids. Electrical and thermal conductivities decreased with increasing ZrO₂ content, attributed to the insulating properties of ZrO₂ particles, which hinder electron and phonon transport. The results suggest the potential application of ZrO₂-reinforced 7075 aluminum alloys in fields requiring mechanical and structural enhancements, such as aerospace, automotive, and energy industries, considering the impact of reduced electrical and thermal conductivities.

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